

6/PR75

METHOD FOR OPERATING AN INTERNAL COMBUSTION ENGINE

Related Art

5 The present invention relates to a method for operating an internal combustion engine of a motor vehicle, in particular, having a control device for controlling/regulating the internal combustion engine as a function of an air-mass sensor signal from a first air-mass sensor.

10 Furthermore, the present invention relates to an internal combustion engine of a motor vehicle, in particular, having a control unit for controlling/regulating the internal combustion engine as a function of an air-mass sensor signal from a first air-mass sensor.

15 The present invention also relates to a control unit for an internal combustion engine of a motor vehicle, in particular, for controlling/regulating the internal combustion engine as a function of an air-mass sensor signal from a first air-mass sensor.

20 If a fault occurs in the air-mass sensor signal of the air-mass sensor itself, known operating methods have the disadvantage that the control/regulation of the internal combustion engine is influenced in such a way that the
25 internal combustion engine will no longer be working in the optimal operating point.

When driving on a wet surface, for instance, spray water may

get into an intake tract of the internal combustion engine where it can penetrate an air filter and wet an air-mass sensor installed in the intake tract. This effect, which is also known as water entry, is particularly disadvantageous in the widely used hot-film air-mass sensors, which have a heating surface that cools spontaneously when coming into contact with water in the liquid phase, with the result that the air-mass sensor signal generated by the air-mass sensor is falsified.

Using the falsified air-mass sensor signal, the control unit controlling/regulating the internal combustion engine calculates an incorrect value for the air-fuel ratio to be set, so that the internal combustion engine is no longer working in the optimal operating point, as mentioned earlier.

Furthermore, the emission values of the internal combustion engine are affected since a portion of the introduced water or the water vapor generated therefrom reaches a combustion chamber of the internal combustion engine, where it displaces a portion of the air quantity required for combustion.

Advantages of the Invention

Accordingly, it is the object of the present invention to provide a method for operating an internal combustion engine that minimizes especially the influence of an interference variable, which affects the air-mass sensor signal, on the regulation of the internal combustion engine.

In a method of the type mentioned in the introduction, this objective is attained in that at least one first auxiliary signal is utilized and that the influence of an interference variable, which affects the air-mass sensor signal, on the regulation of the internal combustion engine is reduced as a function of the first auxiliary signal.

The inclusion of the first auxiliary signal according to the present invention makes it possible for the internal combustion engine to work in the optimal operating point despite a fault in the air-mass sensor signal. Compared to conventional operating methods for internal combustion engines, an optimal power output of the internal combustion engine is ensured even when driving on wet surfaces, and compliance with legally mandated limit values for emissions of the internal combustion engine is given as well.

An advantageous specific embodiment of the operating method according to the present invention is characterized in that a comparison of the first auxiliary signal, or of a signal derived from the first auxiliary signal, with the air-mass sensor signal, or a signal derived from the air-mass sensor signal, is performed and a comparison result is obtained.

Comparing the first auxiliary signal with the air-mass sensor signal makes it possible to conclude a fault of the air-mass sensor in the case of substantially different signal characteristics. In this manner, wetting of the heating surface of a hot-film air-mass sensor with water, for instance, is able to be detected. It is also possible to detect other types of faults of the air-mass sensor, for instance a signal cut-off of the sensor caused by mechanical damage to a signal line.

A direct comparison of a signal derived from the first auxiliary signal with the air-mass sensor signal or also with a signal derived from the air-mass sensor signal is particularly advantageous. This makes it possible to include only certain signal components of the first auxiliary signal in the comparison.

Another specific embodiment of the operating method according to the present invention is characterized in that a controlled variable for the control of the internal combustion engine is

obtained as a function of the comparison result. The use of this controlled variable allows the control/regulation of the internal combustion engine to be adapted in such a way that a compensation of the influence of the disturbance variable on the air-mass sensor signal may take place.

In a very simple variant of the method, the controlled variable may be obtained from the difference of a first auxiliary variable, interpreted as setpoint value for the air mass flowing into the intake tract, and the air-mass sensor signal.

In a further development of this method variant, it is additionally possible to obtain the controlled variable from the first auxiliary signal alone; this is always useful when the air-mass sensor signal deviates significantly from an expected value. When the air-mass sensor is not available at all, the method according to the present invention will still allow the internal combustion engine to be operated in the optimal operating point.

Another advantageous specific embodiment of the operating method according to the present invention is characterized by the first auxiliary signal being obtained from state variables of the internal combustion engine, so that no additional external sensors are necessary to obtain the first auxiliary signal. Instead, the first auxiliary signal may be ascertained from the position of a driver pedal, the rotational speed, the temperature as well as other state variables of the internal combustion engine.

Another, especially advantageous specific embodiment of the present invention is characterized by the first auxiliary signal being obtained from a signal of an exhaust-gas probe such as a lambda probe. In this specific embodiment it is possible to subject the air-mass sensor signal to a plausibility check since, with knowledge of the injected fuel

quantity, the fuel mass actually conveyed to the combustion chamber may be calculated from the signal of the exhaust-gas probe. In contrast to the air-mass sensor signal, the signal of the exhaust-gas analyzer probe is not greatly falsified by the water vapor in the combustion chamber.

If the first auxiliary signal deviates significantly from the air-mass value obtained from the air-mass sensor signal, a malfunction of the first air-mass sensor may be concluded, possibly due to water in the intake tract. In this case, the operating method according to the present invention even makes it possible to discard the faulty air-mass sensor signal and to substitute the first auxiliary signal as input variable for the control device of the internal combustion engine.

To consider the generally higher dynamics of a hot-film air-mass sensor compared to a lambda probe, the measured values of the air-mass sensor signal may be averaged. As an alternative, it is possible to connect a filter downstream from the air-mass sensor, which describes the dynamics of the controlled system of the lambda probe. If the internal combustion engine is a diesel gasoline engine, a lean-mixture sensor may be used as exhaust-gas probe.

It is preferred if a permanent comparison of the air-mass sensor signal with the signal from the exhaust-gas probe takes place within the framework of the afore-described plausibility control of the air-mass sensor signal, the controlled variable for regulating/controlling the internal combustion engine being obtained as a function of the comparison result.

Another advantageous specific embodiment of the operating method according to the present invention is characterized by the comparison including the following steps: differentiating the air-mass sensor signal so as to obtain a differentiated air-mass sensor signal; differentiating the first auxiliary signal to obtain a differentiated auxiliary signal; and

forming the difference from the differentiated air-mass sensor signal and the differentiated auxiliary signal to obtain a differential signal, the differential signal being a measure for the difference in the time change between the signal from the first air-mass sensor and the first auxiliary signal. The first auxiliary signal is preferably obtained from the state variables of the internal combustion engine or from the signal of an exhaust-gas probe and may be interpreted as setpoint value for the air mass.

If the differential signal exceeds a predefinable threshold value, which corresponds to a dynamic response of the air-mass sensor signal that deviates significantly from the first auxiliary signal, a malfunction or a fault of the air-mass sensor is detected in this specific embodiment. It is advantageous for simple processing of the differential signal if the differentiated air-mass sensor signal is scaled to a time average of the air-mass sensor signal, the differentiated auxiliary signal is scaled to a time average of the first auxiliary signal, and the absolute value of the differential signal is generated so as to obtain a positive differential signal. Finally, the differential signal is compared to at least one predefinable threshold value. If the afore-mentioned absolute-value generation is omitted, two threshold values for the differential signal must be selected accordingly.

The threshold value makes it possible to specify the maximum value/the extremal values of the differential signal at which a difference between the air-mass sensor signal and the first auxiliary signal is not yet interpreted as fault of the air-mass sensor signal.

In the case of a single threshold value and in the event that it is exceeded, the first auxiliary signal is obtained as controlled variable. The air-mass sensor signal is obtained as controlled variable if the comparison result indicates that the differential signal is smaller than or equal to the

threshold value. An analogous procedure is proposed in the case of two threshold values.

In a further advantageous specific embodiment of the operating method according to the present invention, the first auxiliary signal is obtained from a signal of a second air-mass sensor. The additional, second air-mass sensor, just like the exhaust-gas probe, allows a plausibility control of the air-mass sensor signal from the first air-mass sensor.

Another advantageous specific embodiment of the present invention provides that the first auxiliary signal be obtained from a signal of an already present rain sensor of the motor vehicle. Rain sensors are used to control windshield wipers, for example, and the signals they provide may be utilized as a measure for the precipitation quantity. From the precipitation quantity, which is correlated to the interference variable influencing the air-mass sensor signal, namely the water quantity striking the heating surface of the hot-film air-mass sensor, the controlled variable may be ascertained.

Another advantageous specific embodiment of the present invention is characterized in that the first auxiliary signal is obtained from a signal of a capacitive sensor, the capacitive sensor being configured as integral component of the first air-mass sensor. A variant having an especially small design results from the fact that the surface of the already present first air-mass sensor is used as first capacitor plate of the capacitive sensor. A second capacitor plate of the capacitive sensor may be arranged in a housing of the first air-mass sensor, for example.

Another advantageous specific embodiment of the present invention is characterized in that the first auxiliary signal is obtained from a signal of an ohmic sensor, the ohmic sensor being configured as integral component of the first air-mass sensor. An especially advantageous specific embodiment of the

method according to the present invention is characterized by the ohmic sensor having at least two electrodes preferably made of a corrosion-resistant material. This ensures that the ohmic sensor is also suited for long-term operation.

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A very advantageous further specific embodiment of the present invention provides for the ohmic sensor to be arranged on the surface of the first air-mass sensor.

10 In an advantageous further development of the operating method according to the present invention, the first auxiliary signal is obtained from the signal of the capacitive sensor and the signal of the ohmic sensor. Water droplets striking the surface of the air-mass sensor are able to be detected in a
15 reliable manner by changes in the capacitance or the conductivity of the respective sensor. If a hot-film air-mass sensor is used, an arrangement of the capacitive/ohmic sensor directly on the heating surface is useful.

20 Within the framework of the comparison, an especially advantageous specific embodiment of the method according to the present invention provides for a difference to be formed from the first auxiliary signal and the air-mass sensor signal so as to obtain the controlled variable. The first auxiliary
25 signal is preferably determined from the state variables of the internal combustion engine, such as the driver-pedal position, the rotational speed and additional variables. The first auxiliary signal in this case represents a setpoint value for the air mass to be conducted to the internal
30 combustion engine, the setpoint value being obtained from the state variables of the internal combustion engine. This allows a comparison with the air-mass signal actually detected by the air-mass sensor.

35 A filtering of the air-mass sensor signal prior to forming the difference is particularly advantageous for obtaining a filtered air-mass sensor signal. In this way, only the signal

frequencies of the air-mass sensor signal that are meaningful for the comparison are considered in the comparison. For example, when a low pass filter is used for filtering, high frequency signal components of the air-mass sensor signal are filtered out and will not be entered in the difference generation.

From measurements it is known that such high frequency signal components of the air-mass sensor signal are produced by water droplets hitting the heating surface of the air-mass sensor and by the related spontaneous cooling of the heating surface.

These high frequency signal components may be considered an interference variable since they do not contain any directly analyzable information about the air mass entering via the intake tract and have an interfering effect on the difference formation and thus on the controlled variable as well. This is prevented by using a low pass filter according to the present invention. It is particularly useful in this context to select the cut-off frequency of the low pass filter such that the low pass filter filters out the highest possible portion of the signal energy of the high frequency signal components so as to minimize the influence of the interference variable.

To this end, an especially advantageous variant of the method according to the present invention provides that the cut-off frequency of the low pass filter be selected dynamically and as a function of state variables of the internal combustion engine. This allows an especially good suppression of the interference variable via the low pass filter. Furthermore, additional interfering signal components of the air-mass sensor signal whose spectrum depends on the operating state of the internal combustion engine may be suppressed in this manner.

A highly advantageous additional specific embodiment of the operating method according to the present invention is

characterized in that the cut-off frequency of the low pass filter is selected as a function of a model of the internal combustion engine. A so-called system model of the internal combustion engine may be used as model, which provides
5 information regarding the spectrum of allowed air-mass sensor signals in the respective state of the internal combustion engine as a function of the state variables of the internal combustion engine.

10 Using this information, the cut-off frequency of the low pass filter is able to be selected in such a way that only spectral components of the air-mass sensor signal that are not caused by an interference effect are entered in the difference formation.

15 A further specific embodiment of the method according to the present invention is characterized in that the first auxiliary signal is obtained from the air-mass sensor signal by filtering with a high pass filter and is used as a controlled
20 variable to control the internal combustion engine.

As already mentioned, it is known that water droplets striking the heating surface of a hot-film air-mass sensor cause high frequency signal components, in particular, which are able to
25 be separated from the low frequency signal components of the air-mass sensor signal by the high pass filter utilized according to the present invention. In this case the first auxiliary signal is a measure for the water quantity striking the air-mass sensor and may be used as controlled variable.

30 In this variant as well, the selection of the cut-off frequency of the high pass must be implemented dynamically and as a function of state variables of the internal combustion engine in order to increase the accuracy of the method,
35 thereby preventing that the first auxiliary signal also contains signal components of a useful signal of the air-mass sensor.

Another specific embodiment of the method according to the present invention is characterized by a second auxiliary signal being obtained from the air-mass sensor signal via filtering with a low pass filter, and by the controlled variable being obtained from the first auxiliary signal, the second auxiliary signal and state variables of the internal combustion engine. In this specific embodiment, the first auxiliary signal constitutes a measure for the water quantity striking the air-mass sensor; the second auxiliary signal constitutes the actual useful signal of the air-mass sensor representing the air mass flowing through the intake tract; and from the state variables of the internal combustion engine it is possible in turn to dynamically select a cut-off frequency of the low pass/high pass filter.

It is conceivable that the cut-off frequency of the low pass filter corresponds to the cut-off frequency of the high pass filter. To obtain a spectral separation of the first and the second auxiliary signal, a band stop may be utilized instead of the low pass filter and the high pass filter, the band stop's lower cut-off frequency matching the cut-off frequency of the low pass filter and its upper cut-off frequency matching the cut-off frequency of the high pass filter.

According to a further advantageous specific embodiment of the present invention, the cut-off frequency of the high pass/low pass filter is selected as a function of a model of the internal combustion engine. As an alternative it is also possible for the upper and the lower cut-off frequency of the band stop to be selected as a function of a model of the internal combustion engine.

Another, especially advantageous specific embodiment of the method according to the present invention in which two air-mass sensors are arranged in an intake manifold of the internal combustion engine in such a way that air flowing into the intake manifold first reaches the first air-mass sensor

and then the second air-mass sensor, which is located at a distance in the flow direction of the aspirated air, includes the following steps within the framework of the comparison: Delaying the air-mass sensor signal by a delay time so as to
5 obtain a delayed air-mass sensor signal; subtracting the first auxiliary signal from the delayed air-mass sensor signal in order to obtain a differential signal; integrating the differential signal so as to obtain an indicator signal; differentiating the delayed air-mass sensor signal to obtain a
10 differentiated air-mass sensor signal; forming the amount of the differentiated air-mass sensor signal to obtain a positive air-mass sensor signal; differentiating the first auxiliary signal to obtain a differentiated auxiliary signal; forming the amount of the differentiated auxiliary signal to obtain a
15 positive auxiliary signal; subtracting the positive auxiliary signal from the positive air-mass sensor signal to obtain an additional differentiated signal.

The indicator signal obtained from the differentiated signal
20 is a measure for the water quantity present in the intake manifold or in the intake tract; and the operational sign of the additional differentiated signal indicates which one of the two air-mass sensors provides the greater signal change. According to the present invention, when a predefinable
25 threshold value for the indicator signal is exceeded, i.e., in the case of water entry into the intake tract, the controlled variable is obtained from the indicator signal and the signal of the particular air-mass sensor for which the smaller signal change has been detected. This mechanism takes the fact into
30 account that high-frequency signal components in the air-mass sensor signal are in all likelihood caused by water droplets striking the heating surface of an air-mass sensor, or originate from other interference effects and not from usually low-frequency changes in the air-mass flow through the intake
35 tract that are appropriate to the operation.

Another advantageous specific embodiment of the method

according to the present invention is characterized in that both air-mass sensors are arranged next to one another; in that the delay step is omitted; and in that the second air-mass sensor is provided with a water-droplet separator. In another method variant according to the present invention it is especially advantageous that a model simulating the dynamic response of the water-droplet separator is taken into account in the processing of the air-mass sensor signal and/or the first auxiliary signal. The model makes it possible to consider the dynamic response of the second air-mass sensor, which is changed because of the water-droplet separator, thereby ensuring the comparability of the sensor signals from the first air-mass sensor and the second air-mass sensor.

Another specific embodiment of the method according to the present invention is characterized by both air-mass sensors being integrated in a shared sensor system, preferably in a shared housing.

Another, especially advantageous specific embodiment of the method according to the present invention is characterized in that the first air-mass sensor is designed as hot-film air-mass sensor.

Of special importance is the implementation of the method according to the present invention in the form of a computer program which is provided for a control unit of an internal combustion engine in a motor vehicle, in particular. The computer program has program codes suitable for carrying out the method according to the present invention when it is executed on a computer. Furthermore, the program code may be stored on a computer-readable data carrier, such as in a so-called flash memory. In these cases, the present invention is thus realized by the computer program, so that the computer program represents the present invention in the same manner as the method for whose execution the program is suitable. As an additional attainment of the object of the present

invention, an internal combustion engine is indicated as recited in Claim 43. Still another attainment of the object of the present invention is given by a control unit as recited in Claim 44.

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Further features, uses and advantages of the present invention come to light from the following description of exemplary embodiments of the present invention, which are shown in the figures of the drawing. In this context, all of the described or represented features, by themselves or in any combination, form the subject matter of the present invention, regardless of their combination in the patent claims or their antecedents, and regardless of their formulation and representation in the specification and drawing, respectively.

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The figures show:

Figure 1 a schematic signal flow chart on which a first specific embodiment of the method according to the present invention is based;

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Figure 1a a flow chart corresponding to the signal flow chart of Figure 1;

Figure 2 a schematic signal flow chart of a second specific embodiment of the present invention;

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Figure 2a a flow chart corresponding to the signal flow chart of Figure 2;

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Figure 3 a signal flow chart of a third specific embodiment of the method according to the present invention;

Figure 4 the arrangement of the hot-film air-mass sensors HFM_1, HFM_2 in intake manifold 4 in a schematic representation, as well as the associated signal flow chart;

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Figure 4a a flow chart of the third specific embodiment of the method according to the present invention; and

Figure 5 an internal combustion engine according to the present invention.

Figure 1 shows a signal flow chart of a first method variant according to the present invention in which a first auxiliary signal H_1 together with an air-mass sensor signal L_1 from a first hot-film air-mass sensor HFM_1 (Figure 5) is analyzed. Air-mass sensor HFM_1 is arranged in intake tract 3 of an internal combustion engine 1 (Figure 5) and emits a signal L_1 whose value is proportional to the air mass flowing through the intake tract.

The evaluation of signals L_1 , H_1 makes it possible to reduce the influence of an interference variable, which affects air-mass sensor signal L_1 , on the control/regulation of internal combustion engine 1 implemented by control unit 2. The time sequence of the method steps for the evaluation may be gathered from the flow chart of Figure 1a.

As can be seen in Figure 1, auxiliary signal H_1 is obtained from the following state variables of internal combustion engine 1: from pressure P of the fresh air outside intake tract 3; from temperature T of the fresh air; and from the rotational speed n of internal combustion engine 1; as well as possibly from additional state variables (not shown) of internal combustion engine 1 as well. Auxiliary signal H_1 indicates the air mass determined from state variables P , T , n with the aid of the general gas equation, the air mass being the air mass required by internal combustion engine 1 during the operation with state variables P , T , n .

First auxiliary signal H_1 is conveyed to differentiator 20, which, in step 211 of the flow chart of Figure 1a, forms a differentiated auxiliary signal H_{1_1} from first auxiliary

signal H_1.

Next, in step 211a of Figure 1a, differentiated auxiliary signal H_1_1 is scaled to a time average H_1_m of first auxiliary signal H_1.

In parallel with steps 211, 211a, air-mass sensor signal L_1 of first air-mass sensor HFM_1 (Figure 5) is transmitted to a further differentiator 21 (Figure 1), which takes place in step 210 of Figure 1a. Differentiator 21 of Figure 1 delivers a differentiated air-mass sensor signal L_1_1, which, in a following step 210a (Figure 1a), is scaled to a time average L_1_m of air-mass sensor signal L_1.

The difference generation from differentiated air-mass sensor signal L_1_1 and differentiated auxiliary signal H_1_1 in subtractor 22 (Figure 1), which follows in step 220, yields a differential signal D_1_1. Finally, in step 230, the amount of differential signal D_1_1 is formed so as to obtain a positive differential signal D_1_1', which is filtered by a filter 23 in following step 240.

Filtered differential signal D_1_1* is compared in a comparator 24 with a predefinable threshold value S_1 in order to obtain a comparison result VE. The comparison of filtered differential signal D_1_1* with predefinable threshold value S_1 takes place in step 250 of Figure 1a.

Two possible comparison results VE exist in comparison 250 with predefinable threshold value S_1 for filtered differential signal D_1_1*, which is always positive due to the amount generation in step 230.

Differential signal D_1_1 indicates the difference between the time change of air-mass sensor signal L_1 of first air-mass sensor HFM_1 and the time change of first auxiliary signal H_1. For as long as differential signal D_1_1 does not exceed

a certain limit value, it is assumed that no interference influence of signal L_1 from air-mass sensor HFM_1 exists. In this case, signal L_1 is obtained as controlled variable R (Figure 1a).

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However, as soon as the limit value is exceeded, it is assumed that an interference influence of signal L_1 is present, which represents the cause of the deviating dynamic response of signals L_1, H_1. In this case, first auxiliary signal H_1 is obtained as controlled variable R, i.e., control unit 2 shown in Figure 5 does not receive a signal L_1 from an external sensor as input variable for the air flowing through intake tract 3, but a variable that is calculated in control unit 2 itself.

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The interference influence may stem from interferences resulting from high-frequency electromagnetic radiation in the area of connecting lines of air-mass sensor HFM_1. Another cause is attributable to water droplets striking the heating surface of air-mass sensor HFM_1 and the spontaneous cooling of the heating surface that accompanies it.

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The described method prevents speed fluctuations or a sudden drop in the output of internal combustion engine 1 and also the exceeding of limit values for the emissions of internal combustion engine 1; this is due to the fact that in a malfunction of air-mass sensor signal L_1, auxiliary signal H_1 is substituted as controlled variable R or as input variable for control unit 2 of internal combustion 1.

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The signal flow chart of a second specific embodiment of the present invention is shown in Figure 2 and simultaneously shows a closed-loop control circuit of internal combustion engine 1. The associated flow chart may be gathered from Figure 2a.

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As can be inferred from Figure 2, air-mass sensor HFM_1

provides an air-mass sensor signal L_1 , which is obtained from the value of the air mass in intake tract 3 of internal combustion engine 1 and an interference variable S_X that is superposed onto this value.

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As already mentioned, interference variable S_X symbolizes signal interferences of air-mass sensor signal L_1 , which are caused, for instance, by water droplets striking the heating surface of air-mass sensor HFM_1.

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According to Figure 2a, signal L_1 is first filtered by a low pass filter 340a in a step 340, which results in a filtered air-mass sensor signal L_1^* . Filtered air-mass sensor signal L_1^* is subsequently subtracted from an auxiliary signal H_1 in a step 380.

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As in the previous example, auxiliary signal H_1 is arithmetically obtained from state variables P , T , n of internal combustion engine 1. Difference generation 380 provides controlled variable R , which is supplied as input variable to control unit 2 and influences the regulation of internal combustion engine 1.

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Controlled variable R acts on a closed-loop control circuit for the exhaust-gas recirculation, for instance. This makes it possible to adjust the air-fuel mixture conveyed to internal combustion engine 1 to an optimal value.

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In the ideal state, controlled variable R assumes the value zero, i.e., the air mass recorded by air-mass sensor HFM_1 is as large as the arithmetically determined air mass of auxiliary signal H_1 . As soon as interference variable S_X assumes a value other than zero, for instance when water enters the intake tract, a non-zero value results for controlled variable R as well.

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To prevent that interference variable S_X influences the

regulation of the exhaust-gas recirculation, air-mass sensor signal L_1 is filtered by low pass filter 340a. On the basis that interference variable S_X usually provides high-frequency signal components compared to the air mass to be measured, in particular when water has entered intake tract 3, the cut-off frequency of low pass filter 340a is selected such that merely all low-frequency signal components of air-mass sensor signal L_1 are allowed to pass and are thus considered when determining controlled variable R. High frequency signal components attributable to the interference variable will not be allowed to pass by 340a and are thus unable to influence the formation of controlled variable R.

It is particularly advantageous to select the cut-off frequency dynamically, i.e., during operation of internal combustion engine 1, that is to say, as a function of a so-called system model of internal combustion engine 1. The system model provides information concerning the spectrum of air-mass sensor signal L_1 as a function of state variables P, T, n., This information also includes the highest signal frequency of signal L_1 to be expected. On the basis of this information it is possible to include in the generation of controlled variable R only that part of the spectrum of signal L_1 that indicates the actually recorded air mass.

Figure 3 shows the signal flow chart of a variant of the present invention, which includes both a high pass filter 440a and also a low pass filter 442a.

On the basis of air-mass sensor signal L_1 of air-mass sensor HFM_1, first auxiliary signal H_1 is obtained from high-pass filtering of signal L_1 using high-pass filter 440a. Second auxiliary signal H_2 is obtained from low-pass filtering of signal L_1 using low pass filter 442a.

Controlled variable R is obtained from the two auxiliary signals H_1, H_2, analogously to the previous examples, from

state variables (not shown in Figure 3) of internal combustion engine 1 (cf. Figure 5).

In this variant, the water quantity in intake tract 3 of internal combustion engine 1 is represented by auxiliary signal H_1, which, due to the high-pass filtering, includes only the signal components stemming from the water droplets striking the heating surface of sensor HFM_1.

The low-frequency signal components of air-mass sensor signal L_1, which indicate the actual air-mass flow, form second auxiliary signal H_2.

The cut-off frequencies of filters 440a, 442a are selected as a function of a model of internal combustion engine 1 and are dynamically adapted to the individual operating state.

With knowledge of the water quantity in intake tract 3 from first auxiliary signal H_1, the actual air mass from second auxiliary signal H_2, and from state variables of internal combustion engine 1 as well as possibly additional parameters of the combustion, it is possible to calculate the air mass actually available in the combustion chambers of internal combustion engine 1.

Even with water in its liquid phase present in intake tract 3 of internal combustion engine 1, it is possible to operate internal combustion engine 1 in the optimal operating point.

Another specific embodiment of the present invention is shown in Figure 4. Two hot-film air-mass sensors HFM_1, HFM_2 are arranged in intake manifold 4 at a clearance D with respect to one another. The arrow symbolizes the flow direction of the air flowing into intake manifold 4.

As can be gathered from Figure 4, first air-mass sensor HFM_1 is first surrounded by an inflowing air volume, and, following

a propagation delay as a function of clearance D, second hot-film air-mass sensor HFM_2 is surrounded by the inflowing air volume as well.

5 First sensor HFM_1 provides air-mass sensor signal L_1 and second sensor HFM_2 provides first auxiliary signal H_1. To compensate for the propagation-delay difference between air-mass sensor signal L_1 and first auxiliary signal H_1 caused by clearance D, timing element 510a is provided. It
10 delays (cf. flow chart Figure 4a) air-mass sensor signal L_1 by the time required by an air volume flowing into intake manifold 4 to travel from first sensor HFM_1 to second sensor HFM_2 and provides delayed air-mass sensor signal L_1_delta_T, which is subsequently differentiated in differentiator 540a so
15 as to obtain a differentiated air-mass sensor signal L_1_delta_T_1. The delay time of timing element 510a is adjustable and is selected such that the difference from signals L_1_delta_T and H_1 is zero when no water is present in intake manifold 4.

20 First auxiliary signal H_1 provided by second sensor HFM_2 is differentiated in differentiator 542a to obtain a differentiated auxiliary signal H1_1. Both differentiators 540a, 542a also perform an amount generation, so that a
25 positive air-mass sensor signal L_1_delta_T_1' and a positive auxiliary signal H1_1', respectively, is present at the individual output.

30 Finally, positive auxiliary signal H1_1' is subtracted from positive air-mass sensor signal L_1_delta_T_1' in order to obtain a further differential signal Z_Diff.

Furthermore, first auxiliary signal H_1 is subtracted from delayed air-mass sensor signal L_1_delta_T, and resulting
35 differential signal D_L_H is integrated in integrator 530a so as to obtain an indicator signal A_L_H.

The indicator signal is a measure for the deviation of the signals measured by sensors HFM_1, HFM_2; from this deviation it is possible to conclude the water quantity introduced in intake manifold 4. Differential signal Z_Diff indicates which one of the two sensors HFM_1, HFM_2 detects a greater signal change.

As soon as indicator signal A_L_H exceeds a predefinable threshold value, controlled variable R (not shown in Figure 4) is obtained either from air-mass sensor signal L_1 or from first auxiliary signal H_1.

To obtain the most reliable value for the measured air mass for forming controlled variable R, the sensor signal whose signal change is smaller is used to form controlled variable R in this case.

If differential signal $Z_Diff > 0$, the signal change of air-mass sensor signal L_1 is greater than the signal change of first auxiliary signal H_1; in this case, air-mass sensor signal L_1 is ignored and controlled variable R is generated from first auxiliary signal H_1. In an analogous manner, controlled variable R is formed from air-mass sensor signal L_1 in a negative differential signal Z_Diff.

With the aid of indicator signal A_L_H from which the introduced water quantity may be concluded, and using the individual, not ignored sensor signal as a measure for the actual air quantity in intake tract 3, controlled variable R is able to be formed so as to calculate the correct fuel quantity to be injected as a function of the air mass actually available in the combustion chamber.

Both air-mass sensors HFM_1, HFM_2 may also be arranged next to one another in intake manifold 4, second air-mass sensor HFM_2 being provided with a water separator (not shown). Since the water separator modifies the dynamic response of second

air-mass sensor HFM_2, a model of the dynamic response of the water-droplet separator must be connected downstream from first air-mass sensor HFM_1 in order to ensure comparability of the two sensor signals.

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In this variant, a deviation of the sensor signals of both air-mass sensors HFM_1, HFM_2 provides a measure for the water quantity that has entered intake manifold 4. Both air-mass sensors HFM_1, HFM_2 are preferably arranged in the same housing.

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